### Appendix A: Geomorphic Assessment Field Forms

#### A1. Channel-stability Ranking Scheme field form (CSRS)

#### **CHANNEL-STABILITY RANKING SCHEME\***

Station #					Sheet #	::
Date:		_Crew:		Site Coordinate	es:	
Pictures:	□ U/S □ D/S	☐ X-section ☐ L	в 🗖 кв	Samples:		
Pattern:	☐ Meandering	☐ Straight ☐ Br	raided 🖵 Drai	-		
Field Mea	surements:	Reach length:		_ Est. Reach Slope		
i icia ilica		_				
	Avg channe			_ Avg/Max channel	-	
				_ RB angle (avg):		
=		<b>-</b>		_ Primary bed mate		
BHS Note #	<del>†</del>		(GP=gravel; SP=sar	nd; ML=silt; CL=clay; BR	=bedrock)	
1. Primar	y bed material	l				
	Bedrock	Boulder/Cobble	Gravel	Sand	Silt/Clay	
	0	1	2	3	4	
2. Bed Pr	otection					
a)	Yes					
OR	0		#Banks			
b)	No	(with)	Protection	One (L or R)	Both	
٥	1			2	3	
3. Degree	-	-	,	vation of "normal" low wa		30%)
	0-10% 4	11-25% 3	26-50% 2	<i>51-75%</i> 1	76-100% 0	
4 Dograd	•	-	<del>-</del>	•	-	
4. Degree	0-10%	11-25%	26-50%	dth from up to down 51-75%	76-100%	
	0	1	2	3	4	
5. Stream		(Each bank over rea				
	None		Mass wasting (	failures)		
Left	0	1	2			
Right	0	1 **** (Danasa) of acad	2			
6. Stream	ı bank instabili 0-10%	ity (Percent of each 11-25%	n bank falling ov <i>26-50%</i>	er reach length) 51-75%	76-100%	
Left	0-10%	0.5	20-30% 1	1.5	2	
Right	0	0.5	1	1.5	2	
J	_		(Percent of eac	h bank face over rea	_	
otabii	0-10%	11-25%	26-50%	51-75%	76-100%	
Left	2	1.5	1	0.5	0	
Right	2	1.5	1	0.5	0	
8. Occurr	ence of bank/b	oar accretion (Per	rcent of each ba	ank with fluvial depos	sition over reach leng	gth)
	0-10%	11-25%	26-50%	51-75%	76-100%	
Left	2	1.5	1	0.5	0	
Right	2	1.5	1	0.5	0	
9. Stage of		olution (If applicab	•			
I	II	III	IV.	V	VI	
0	1	2	4	3	1.5	
OTHER OBS	SERVATIONS:					
					Total Score:	
						·

<sup>\*</sup> Adapted from Kuhnle and Simon (2000)

#### A2a. Biological/Habitat Ranking Scheme (low gradient) form (BHRS-low)

#### **BIOLOGICAL/HABITAT RANKING SCHEME (low gradient streams)\***

Station #		Station Description:			
Date:		Crew:	Samples Taken:		
Pictures:	☐ U/S: ☐ LB ☐	RB	☐ Channel Bed	<b>_</b>	
	D/S: LB	RB	LB Riparian Zone	<b></b>	
			RB Riparian Zone		
			TID Ripanan Zone		
1. Avai	lability of favorable >50%	habitat (snags, subme	erged logs undercut bank 10-30%	s; average of LWD and <10%	detritus)
	4	3	2	1	
2. Pool-	-substrate composi	-	2	,	
	GP & firm SP		All ML-CL or All SP	Hardpan/ Bedrock	
	4	3	2	1	
3. Pool-	-variability characte	er			
	Mix large/small &	Majority large-deep	Shallow pools more	Majority small-	
	deep/shallow	pools	prevalent	shallow or absent	
	4	3	2	1	
4. Activ	e streambed/bar de	eposition			
	0-20%	21-50%	51-80%	81-100%	
	4	3	2	1	
5. Strea	ambed exposure	E 050/	05.750/	<b>7</b> E 4000/	
	0-5%	5-25% 3	25-75% 2	75-100% 1	
6 Dogr	ee of "hard" chann	-		•	ion/soment)
o. Degi	Channelization/dred		zation, dredging, embankmei 40-80% reach	>80% Disrupted/	ion/cement)
	ing absent	William of Thotolio	disrupted	habitat altered	
	4	3	2	1	
7 (low).	Sinuosity				<u> </u>
	3-4	2-3	1-2	Straight	
	4	3	2	1	
7 (high)	. Pool-riffle sequen				
	>80%	51-80%	20-50%	<20%	
	4	3	2	1	
8. Bank	Instability (Percent e		24 000/	04 4000/	
Lef	0-5% t 2	<i>6-30%</i> 1.5	31-60% 1	61-100% 0.5	
Righ	-	1.5	1	0.5	
_	etative Bank Protect		ı	0.5	
J. Vege	>90% covered	70-90% cover	50-70% cover;	<50% veg	
	w/mix of veg.		disruption obvious; bare patches	disruption high	
Lef		1.5	1	0.5	
Righ		1.5	. 1	0.5	
10. Rip	arian-zone width (ou			F	
	>20m	10-20 m	5-10 m	<5m	
Lef		1.5	1	0.5	
Righ	t 2	1.5	1	0.5	
				Total Score	.]

A2b. Biological/Habitat Ranking Scheme (high gradient) form (BHRS-high)

#### BIOLOGICAL/HABITAT RANKING SCHEME (high gradient streams)\*

Station #		Station Description:			
Date:		Crew:	Samples Taken:		
Pictures:	U/S: LB L	RB	☐ Channel Bed	<b></b>	
	□ D/S: □ LB □ I	RB	LB Riparian Zone		
			RB Riparian Zone		
			TID Ripanan Zone		
1. Availa	bility of favorable	habitat (snags, subme	erged logs undercut bank	s: average of LWD and o	detritus)
	>70%	70-40%	40-20%	<20%	1011/1010)
	4	3	2	1	
2. Embe	ddedness: Gravel,	cobble, boulder %	surrounded by fir	ne sediment	,
	0-25%	25-50%	50-75%	>75%	
	4	3	2	1	
3. Veloc	ity/Depth Regime:	a) slow-deep, b) slow-sl m/s, deep is >0.5 m)	nallow, c) fast-deep, d) fa	st shallow; (slow is <0.3	
	All 4 regimes	3 of 4 regimes(if 'd'	2 of 4 regimes (if 'd'	Dominated by 1	
	present	is missing,score	and 'b' missing,	regime (usually 'a')	
		lower	score lower		
	4	3	2	1	
4. Active	e streambed/bar de		20 500/	- F00/	
	<5% 4	5-30%	30-50%	>50%	
5 Stroat	mbed exposure	3	2	1	
J. Sileai	0-5%	5-25%	25-75%	75-100%	
	4	3	20-70%	1	
6 Degre	•	-	zation, dredging, embankme	nte/ehorina etructuree laahi	on/cement)
o. Dog.o	Channelization/dred	Minor or historic	40-80% reach	>80% Disrupted/	on coment)
	ing absent		disrupted	habitat altered	
	4	3	2	1	
7 (high).	Pool-riffle sequen	ce (% Pool + % Riffle)			
	>80%	51-80%	20-50%	<20%	
	4	3	2	1	
8. Bank	Instability (Percent ea	ach bank failing)			
	0-5%	6-30%	31-60%	61-100%	
Left	2	1.5	1	0.5	
Right	2	1.5	1	0.5	
9. Veget	ative Bank Protect		F0 70% 201/27	F00/	
	>90% covered w/mix of veg.	70-90% cover	50-70% cover; disruption obvious;	<50% veg disruption high	
		4 =	bare patches		
Left	2	1.5	1	0.5	
Right	2	1.5	1	0.5	
iu. Kipa	<b>rian-zone width</b> (ou >20m	it from eage of wate 10-20 m	r) 5-10 m	<5m	
Left	2	1.5	1	0.5	
Right	2	1.5	1	0.5	
Nigit	۷	1.5	I	0.5	
				Total Score:	

#### A3. Bank Height/Slope Measurement Notes form (BHS), page 1

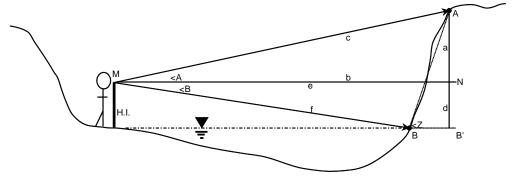
#### BANK HEIGHT/SLOPE (BHS) MEASUREMENT NOTES

NOTE #:	DATE:	CREW:	UNITS: Metric / English		
STREAM:	TIME:	REACH LOCATION:			
CROSS-SECTION#	of	DISTANCE FROM U/S REACH:			
Measurement instrument	s:				
Distance method:	tape / laser rangefinder / ac	finder / acoustic device / pace / other			
Inclination method:	Abney level / Brunton / cli	Abney level / Brunton / clinometer / hypsometer / rod & tape / other level			

Cross-section sketch for instrument and shot locatio	ns (see examples):
LB	RB

STANDING	Location of	Location of	I I			Height
ON BANK	Target on	Instrument	Height of	Distance	Angle	from Level
(Left/Right) Shot ID	Bank*	*	Instrument	(indicate units)	(degrees)	(M-N)
A	<u> </u>					
В						
<d< td=""><td><u>i                                     </u></td><td></td><td></td><td></td><td></td><td></td></d<>	<u>i                                     </u>					
3	<u>i</u>		L			; 
4						[
5	·	[ 	i L	i		[ ]
6	l .J.,	) 	l 	I 	 <del> </del>	I <del> </del>
1	1		! !			] 
		Scenario #2	1			
	(A, B)	$(A, B, \langle D)$	1	2	3	4
Ht of Opposite Bank	:J	<u> </u>	!			
Angle of Opposite Bank	:		l			1
Ht of Near Bank		[	<b></b>			[
Angle of Near Bank		)	/ <del></del> /			,
Channel Width @ TOB	:		l		İ	I

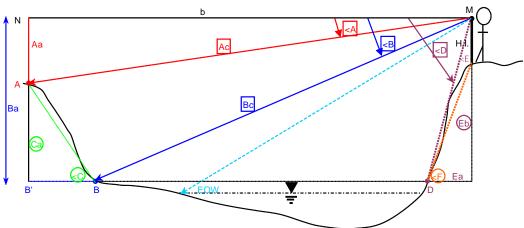
<sup>\*</sup> TOB/VF=lop of bank/vertical face; UB=upper bank; SL=slough line; DS=deposition surface; EOW=edge of water; CB=cutbank; CS/Bar=channel shelf



#### Measure:

- 1) Shoot points A and B with rangefinder to get lengths c and f.
- 2) Measure <A and <B with level to get inclination in degrees.

a + d = (c \* sin < A) + (f \* sin < B)Height of Bank (Distance AB'): Average Slope of Bank (in degrees):  $\tan < Z = \underline{a + d}$ 



#### Measure:

- 1) Shoot points A and B with rangefinder to get lengths Ac and Bc.
- 2) Measure <A, <B, and <D with level to get inclination in degrees.

Ba = Bc \* sin<B Height of Opposite Bank (Distance AB'=Ca):

Aa = Ac \* sin<A

Ca = Ba-Aa

Average Slope of Opposite Bank (in degrees): <C = 90-(tan-1 [Ca / (A-B)])

Height of Near Bank (Eb): **Eb** = Ba - H.I. Average Slope of Near Bank (in degrees):

<E = 90 - <D

Ea = Ba \* tan<E

 $<\mathbf{F} = 90$ -(tan-1 [Fh/Fa])

 $b = \sqrt{(Ac^2 - Aa^2)}$ 

Drawings adapted and modified from Compton (1962).

Channel Width at TOB (b):

#### Geomorphic Assessment Stream-Evaluation Data Sheet

Adapted from Kuhnle a SITE INFORM	and Simon (2000), Rhoad ATION	998)	☐ Metric	☐ English		
STATION#:		DATE:	CREW:	EVALUATION SHEET #:		
SITE NUMBER:	STREAM NAME	Ξ:		MAJOR WATER	SHED:	
NEAREST GAG	ING STATION:	DRAINAGE AR	EA:	COUNTY:		
QUAD SHEET:		COORDINATES	(Lat/Long or TR	S):		
WEATHER (current):			WEATHER (pas	t 24 hours):		
GENERAL STE	REAMFLOW CO	NDITIONS				
FLOW TYPE:		FLOW WIDTH:		FLOW DEPTH:		
(none smooth pool/rif	fle, run, rapid-tumbling)			(@ center)		
APPEARANCE		AVG SURFACE	VELOCITY:	FLOW (cfs):		
				(if available or [high, m	andium lowel)	
HIGH FLOW PL	ANFORM:			SINUOSITY:	ictium, iow j)	
(atmight mildly sinner	a mandarina tartuana	hmidad anahmanahina)		Control of the Contro		
LOW FLOW PLA	s, meandering, tortuous,	, oranged, anaorancining)		(channel length/valley length)  SINUOSITY:		
	s, meandering, tortuous, ANNEL DESCRI			(channel length/valley l	length)	
REACH LENGTH		TOP-BANK WII	OTH:	U/S end:		
		Mid Reach:		D/S end:		
MAXIMUM CH.	ANNELWIDTH		and CORRESPO	NDING		
(for entire reach):			CHANNEL DEPTH:			
MAXIMUM CHA	NNEL DEPTH		and CORRESPONDING			
(for entire reach):			CHANNEL WIL	TH:		
GRADIENT:	STRUCTURES:			%DETRITUS:	%LWD:	
	(none, bridge, grade co	ntrol, culverts, bank)				
% POOL:	% RIFFLE:	% RUN:	CROSS SECTIO	N TAKEN (yes / 1	10)?	
	(Pool + Riffle + Run =		Location of Record:	20002000 200		
BED WIDTH:	Method:	BERM WIDTH:	Method:	CEM:		
(Method:	T=tape, R=rangefinder	(type); A=acoustic device	ce, P=pace)	(I, II, III, IV, V, VI)		
BANKFULL INI	DICATORS (circle	e any): none-incis	ed / active floodpl	ain / berm / woody	veg / bar tops	
% RELATIVE E			% RELATIVE EI			
BANKFULL:			LOW WATER:			
		p height = 100%, N/A if				
manufacture out to be a second	IRIAN ZONE (Top		Not the following of the commence	ARIAN ZONE (Top		
of Left Bank):	ANDLISE (urban	, forest, pasture, ro	of Right Bank):	uffer-width)		
Left:	/ (I Com (urban,	, 1010st, pasture, 10	Right:	,	1	
	· · · · · · · · ·		B			

#### CHANNEL BED DESCRIPTION

BED MORPHOLOGY:		BED CONTROLS	i:
(flat, uniform; scour holes; pool-riffle sequence)			e materials; armoured; structure; rip-rap)
PRIMARY BED-MATERIAL TYPE:		SECONDARY BE	D-MATERIAL TYPE:
	(GP=gravel; SP=sand; N		
POOL SUBSTRATE:		ACTIVE BED DE	SPOSITION (Type and % area):
(GP with firm SP; Soft SP with ML-CL; All ML CL; Rock)	CL; All SP; Hard Pan	(GP-SP, SP, ML, CL)	
BED EXPOSED:	EXPOSED BED	FORMS:	COHESION (kg/cm <sup>2</sup> ):
,	(attached point bar, mid		(shear testing device; 14.2258)
KNICKPOINT PRESENT?	HEIGHT:	MATERIAL:	
(Yes / No)		(GP, SP, ML, CL, BR)	
Planform Sketch:		_	
u's limit d'e limit Study Reach Limits     North Pe	Map Symb	Cut Bank	Photo Point ⊕→
Cross-section A—A' Flow Dir Bank Profile	rection	Exposed Island/Bar	Photo Point Sediment Sampling Point Significant Vegetation
Dank Frome	ig riow ¥ ¥	oraciare	∑ oigimeant vegetation Q±1
SEDIMENT SAMPLES:	СН	СН	СН

#### LEFT BANK DESCRIPTION

REACH TYPE:		BANK HEIGH	Γ:		BANK ANGLE (d	egrees):
(I=inside; O=outside; S=straigl	ht	(average or range)			(average; degrees from	horizontal)
% WOODY COVER:		% HERBACEO	US COVER:		% OTHER:	,
DENDROGEOMORPI	HIC INDICA	TORS [corrasion	scars/tilt sprout	s/tree ag	e/tree ring anomalies]	(circle):
BANK SURFACES (y	es, no):					
VF UB_		SL	DS		CB	CS/Bar
(VF=vertical face; UB=upper						
HEIGHT OF CB: HEIG	3HT OF VF:		SION CRAC	K	SHEAR STRENG	GTH (kg/cm <sup>2</sup> ):
		FROM VF:			(shear testing device; 1-	1 2258)
SURFICIAL MATERIA	L (Origin / T	[vne]:			(shear testing device, 1-	1.2236)
VF / UB	/	SL /	DS /		CB /	CS/Bar /
(I=insitu [M=modern; PM=pre-mo	dern], D=deposited					
TYPE OF ACCRETED	)	% BANK WITH			% BANK	
SEDIMENT:		FLUVIAL			FAILING:	
(N=none, CL=clay, ML=silt, SP=s	and, GP=gravel)	DEPOSITION:				
DOMINANT TYPE OF	EROSION F	PROCESS ON:				
VFUB_		SL	DS		CB	CS/Bar
(N=none-stable, MW=mass w. Bank Sketch:	asting, F=fluvial					
	Bank Tan Edea	_⊬ ⊬	ofile Symbol Failed Debris	ls L	Facinessad Stanton	
	Bank Top Edge Bank Toe		Attached Bar	P .	Engineered Structure Significant Vegetation	Q±
	Water's Edge	- Kright	Undercutting		Vegetation Limit	Office
SEDIMENT SAMPLE	C.	LB	LB		LB	LB
SEDIMENT SAMPLE	S.	LD	LD		LD	LD

March 2004, v. 4, L. Keefer

Page \_\_\_ of 5

#### RIGHT BANK DESCRIPTION

% WOODY COVER:  % HERBACEOUS COVER:  % OTHER:  DENDROGEOMORPHIC INDICATORS [corrasion scars/tilt sprouts/tree age/tree ring anomalies] (circle):  BANK SURFACES (yes, no):  VFUBSLDSCBCS/Bar	(I=inside; O=outside; S=straig	ht	(average or range)		,	,
### WOODY COVER:  ### WOOTHER:  ### WOODY COVER:  ### WOOTHER:  ### WOODY COVER:  ##		ht			(average; degrees from	horizontal)
### WOODY COVER:  ### WOOTHER:  ### WOODY COVER:  ### WOOTHER:  ### WOODY COVER:  ##					(areange, aegrees areas	
DENDROGEOMORPHIC INDICATORS [corrasion scars/tilt sprouts/tree age/tree ring anomalies] (circle):  BANK SURFACES (yes, no):  VF	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			IS COVER:	l% OTHER:	
BANK SURFACES (yes, no):  VF UB SL DS CB CS/Bar  (VF=vertical face; UB=upper bank; SL=slough line; DS=depositional surface; CB=cutbank; CS/Bar=channel shelf)  HEIGHT OF CB: HEIGHT OF VF: DIST. OF TENSION CRACK SHEAR STRENGTH (kg/cm²):  FROM VF: (shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type):  VF / UB / SL / DS / CB / CS/Bar / (I=insitu [M=modem; PM=pre-modem], D=deposited, F=failed) / (CL=clay, ML=silt, SP=sand, GP=gravel, BR=bedrock)  TYPE OF ACCRETED % BANK WITH % BANK  SEDIMENT: (N=none, CL=clay, ML=silt, SP=sand, GP=gravel) DEPOSITION:  DOMINANT TYPE OF EROSION PROCESS ON:  VF UB SL DS CB CS/Bar  (N=none-stable, MW=mass wasting, F=fluvial erosion, S=sapping, D=deposition)  Bank Sketch: Profile Symbols  Failed Debris Stattached Bar Significant Vegetation Of the position of the profile symbols  Engineered Structure Significant Vegetation Of the position of the position of the profile symbols Significant Vegetation Of the position of the			/ TIBRETOE	ob CO / Em.	/ O THERE.	
VFUBSLDSCBCS/Bar	DENDROGEOMORP	HIC INDICA	TORS [corrasion s	cars/tilt sprouts/tree ag	ge/tree ring anomalies]	(circle):
VFUBSLDSCBCS/Bar						
(VF=vertical face; UB=upper bank; SL=slough line; DS=depositional surface; CB=cutbank; CS/Bar=channel shelf)  HEIGHT OF CB: HEIGHT OF VF: DIST. OF TENSION CRACK FROM VF: (shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type): (Shear testin	BANK SURFACES (y	es, no):				
HEIGHT OF CB: HEIGHT OF VF: DIST. OF TENSION CRACK FROM VF: (shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type):  VF						CS/Bar
FROM VF:  (shear testing device; 14.2258)  SURFICIAL MATERIAL (Origin / Type):  VF						
SURFICIAL MATERIAL (Origin / Type):  VF _ / _ UB _ / _ SL _ / _ DS _ / _ CB _ / _ CS/Bar _ / _ (I=insitu [M=modem; PM=pre-modern], D=deposited, F=failed) / (CL=clay, ML=silt, SP=sand, GP=gravel, BR=bedrock)  TYPE OF ACCRETED	HEIGHT OF CB: HEI	GHT OF VF:	DIST. OF TENS	ION CRACK	SHEAR STRENG	GTH (kg/cm <sup>2</sup> ):
SURFICIAL MATERIAL (Origin / Type):  VF			FROM VF:			
VF / UB / SL / DS / CB / CS/Bar / (I=insitu [M=modem; PM=pre-modem], D=deposited, F=failed) / (CL=clay, ML=silt, SP=sand, GP=gravel, BR=bedrock)  TYPE OF ACCRETED	GLID FIGURE 1				(shear testing device; 1-	4.2258)
(l=insitu [M=modem; PM=pre-modem], D=deposited, F=failed) / (CL=clay, ML=silt, SP=sand, GP=gravel, BR=bedrock)  TYPE OF ACCRETED						
TYPE OF ACCRETED  SEDIMENT: (N=none, CL=clay, ML=silt, SP=sand, GP=gravel)  DEPOSITION:  DOMINANT TYPE OF EROSION PROCESS ON:  VFUBSLDSCBCS/Bar						CS/Bar/
SEDIMENT: (N=none, CL=clay, ML=silt, SP=sand, GP=gravel)   DEPOSITION:   FAILING:   DOMINANT TYPE OF EROSION PROCESS ON:   VF				AL=silt, SP=sand, GP=grave		
(N=none, CL=clay, ML=silt, SP=sand, GP=gravel)   DEPOSITION:    DOMINANT TYPE OF EROSION PROCESS ON:   VF		)			I	
DOMINANT TYPE OF EROSION PROCESS ON:  VF UB SL DS CB CS/Bar  (N=none-stable, MW=mass wasting, F=fluvial erosion, S=sapping, D=deposition)  Bank Sketch:  Profile Symbols  Bank Top Edge Bank Toe Failed Debris Significant Vegetation  Attached Bar Significant Vegetation					FAILING:	
VFUBSLDSCBCS/Bar						
(N=none-stable, MW=mass wasting, F=fluvial erosion, S=sapping, D=deposition)  Bank Sketch:  Profile Symbols  Bank Top Edge Bank Toe Bank Toe Attached Bar Attached Bar Significant Vegetation		EROSION I				
Bank Sketch:  Profile Symbols  Bank Top Edge Bank Toe Bank Toe Attached Bar Significant Vegetation Significant Vegetation					СВ	CS/Bar
Bank Top Edge Failed Debris Engineered Structure Bank Toe Attached Bar Significant Vegetation		asting, F=fluvial				
Bank Toe Attached Bar Significant Vegetation	Bank Sketch:		Pr	-		
			<u> </u>			
			-King			
				_		
	SEDIMENT SAMPLE	ES:	RB	RB	RB	RB

March 2004, v. 4, L. Keefer

Page \_\_\_ of 5

## PHOTOGRAPHIC RECORD CAMERA TYPE: PHOTOGRAPHER: DATE: PHOTO CHECKLIST: STATION #: Remember: add a recognizable scale in U/S ☐ Mid-reach $\square$ D/S all pictures; record photo number; and ☐ Channel Bed ☐ Left Bank ☐ Right Bank time of day (shadows) ☐ Structures RB Riparian LB Riparian РНОТО# DESCRIPTION MISCELLANEOUS OBSERVATIONS

March 2004, v. 4, L. Keefer

Page \_\_\_ of 5

FIELD CHECK	LIST		
П	Binoculars		Map: Air Photos
		H	*************************************
٢	Bottled water	_	Map: Bedrock
	Calculator	Ц	Map: Plat (landowner info)
	Camera (preferrably digital)		Map: Road atlas
	Cell phone		Map: Surficial materials
	Clipboard (field sheets)		Map: Topographic
	Compass (Silva/Brunton)		Measuring tape/stakes/pins
	Field backpack		Pocket Rod/Surveying Rod/Range Pole/Staff
	Field book		Probe rod (tile probe, etc.)
	Field Sheets		Raingear
	First-aid kit (small)		Soil Probe (bank sampling)
	Geologic hammer		Trenching tool/plastic bags/permanent marker
	Grain size chart		Wading boots
	Gravelometer		
	Handheld GPS		
	Increment borer		
	Insect repellent		
	Laser rangefinder / Hypsometer		
	Level (Abney level/clinometer)		

#### Material Size Classification:

(more than 5	5.50	SE-GRAINED SOILS erial is larger than No. 200 sieve size.)
	Clean (	Gravels (Less than 5% fines)
GRAVELS	GW	Well-graded gravels, gravel-sand mixtures, little or no fines
More than 50% of coarse	S GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines
fraction larger	Gravel	s with fines (More than 12% fines)
than No. 4 sieve size	GM	Silty gravels, gravel-sand-silt mixtures
	GC	Clayey gravels, gravel-sand-clay mixtures
	Clean	Sands (Less than 5% fines)
SANDS	sw	Well-graded sands, gravelly sands, little or no fines
50% or more of coarse	SP	Poorly graded sands, gravelly sands, little or no fines
fraction smaller	Sands	with fines (More than 12% fines)
than No. 4 sieve size	SM	Silty sands, sand-silt mixtures
	sc	Clayey sands, sand-clay mixtures

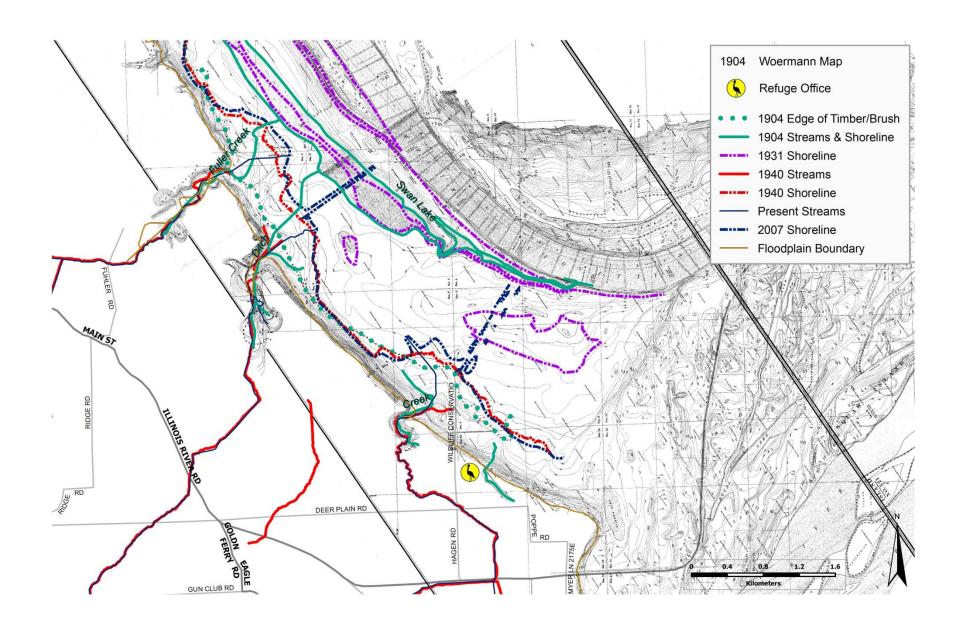
(50% or m	ore o		GRAINED SOILS ial is smaller than No. 200 sieve size.)				
SILTS AND CLAYS Liquid limit less than		ML	Inorganic silts and very fine sands, rock flour, silty of clayey fine sands or clayey silts with slight plasticity				
		CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays silty clays, lean clays				
50%		OL	Organic silts and organic silty clays of low plasticity				
SILTS		мн	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts				
CLAYS Liquid limit 50%		СН	Inorganic clays of high plasticity, fat clays				
or greater		он	Organic clays of medium to high plasticity, organic silts				
HIGHLY ORGANIC SOILS	4 1	PT	Peat and other highly organic soils				

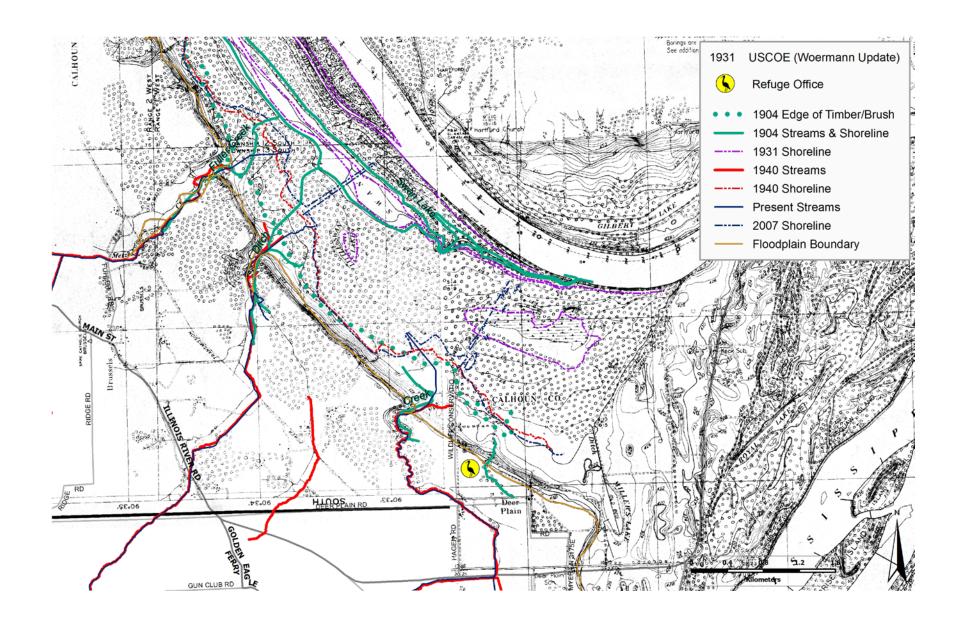
March 2004, v. 4, L. Keefer

Page \_\_\_ of 5

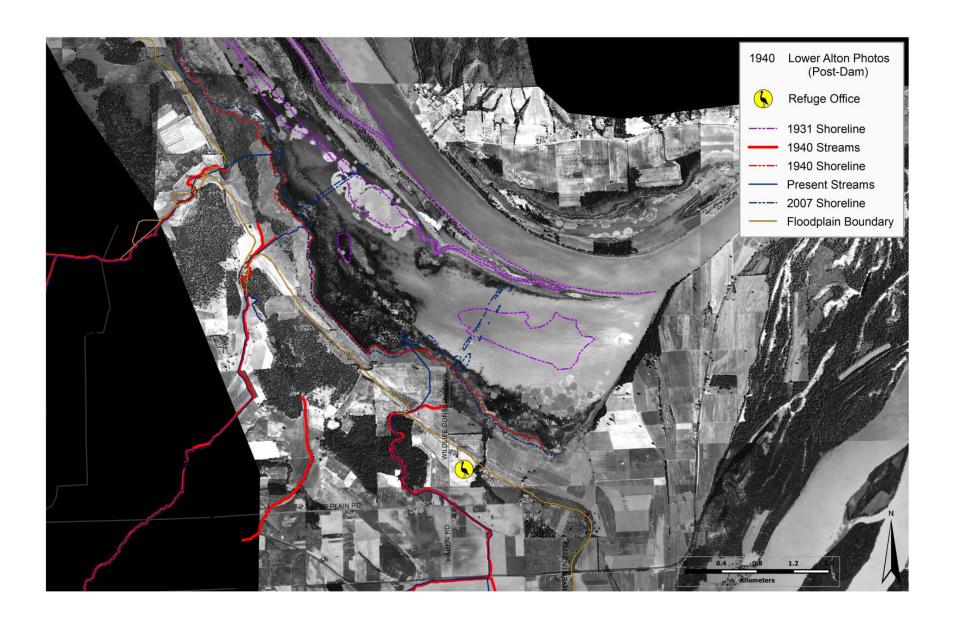
# Appendix B: Historical Aerial Imagery of Swan Lake

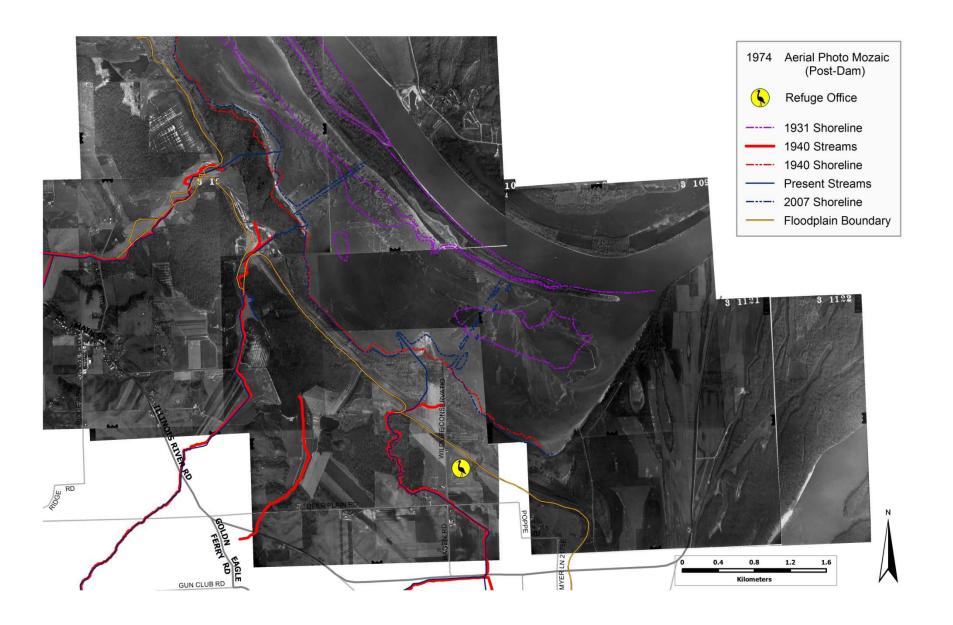
Year (Date)	Source Agency/Program	Type Media
1902-1904	Woermann - USCOE	Drawn maps
1931 (Oct. 25)	USCOE (Woermann update)	Drawn maps (updated with 1931 aerial photography)
1931 (Oct. 25)	Upper Midwest Environmental Science Center, Wisconsin; Lower Alton Pool	Aerial photography
1940 (Jun. 19)	Upper Midwest Environmental Science Center, Wisconsin; Lower Alton Pool	Aerial Photography
1974 (Dec. 9)	Aerial Photo Mozaic	Aerial Photography
1999 (Mar. 25)	USGS	Digital Ortho Quads
2004, 2005, 2006, 2007, and 2009 (Agricultural growing season)	USDA – National Agricultural Imagery Program (NAIP)	Digital Ortho Quarter Quads

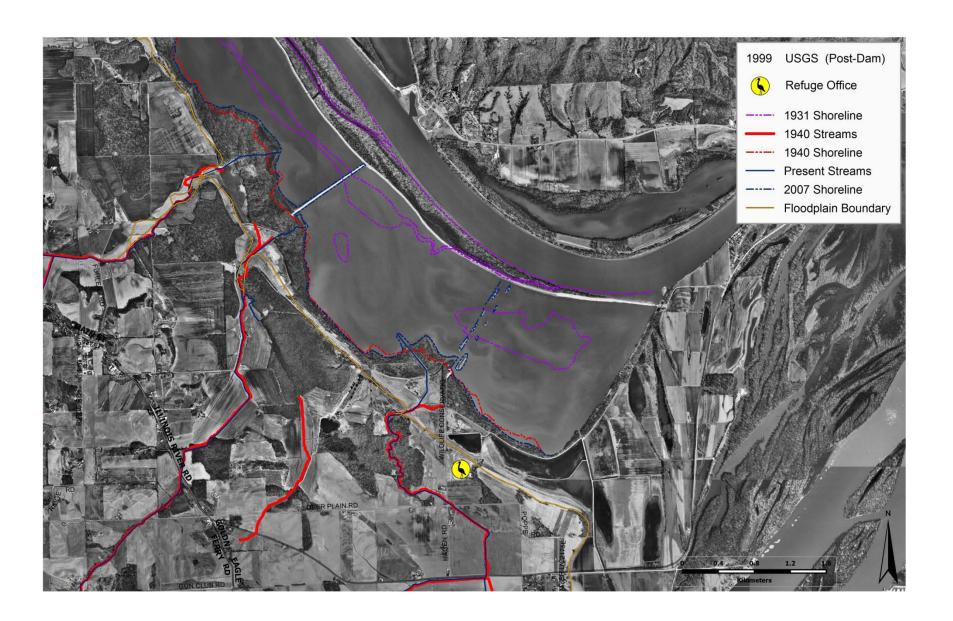


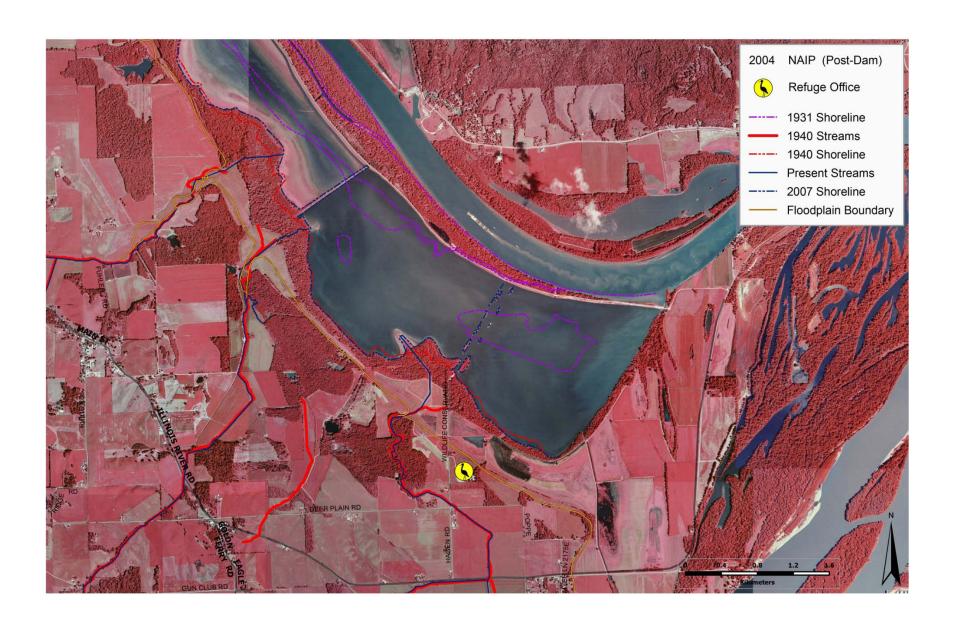


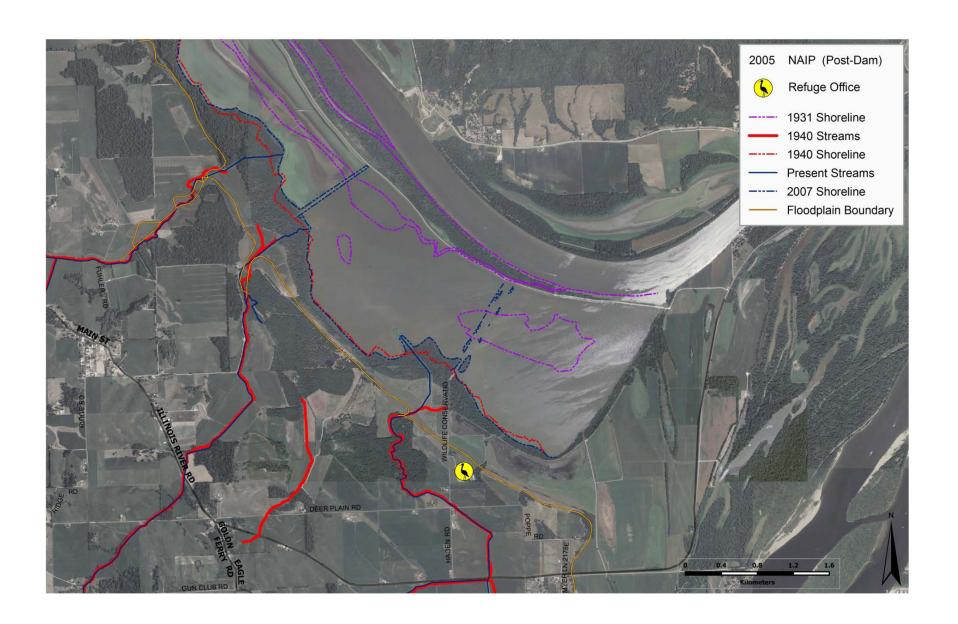


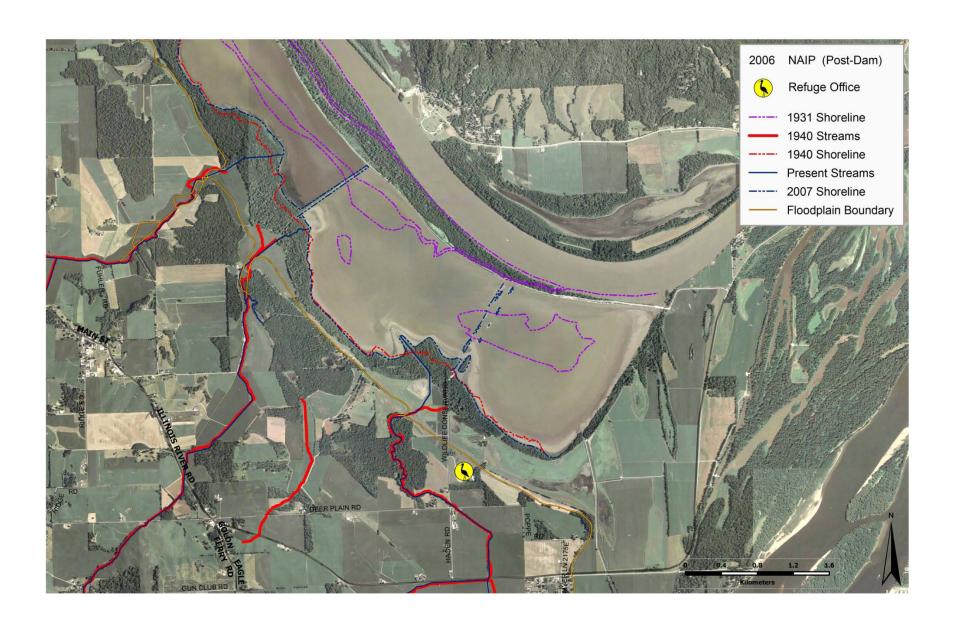


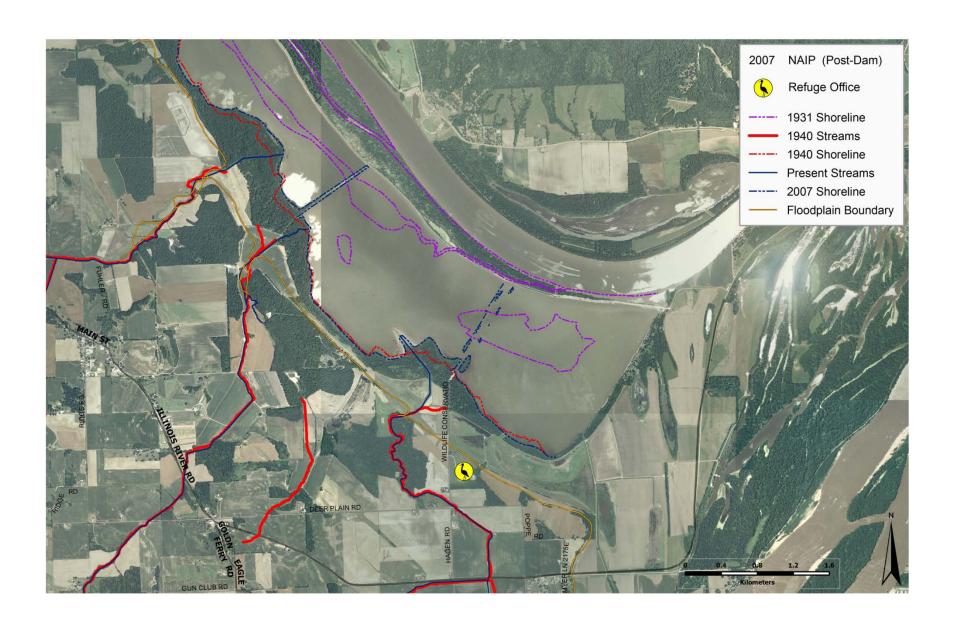


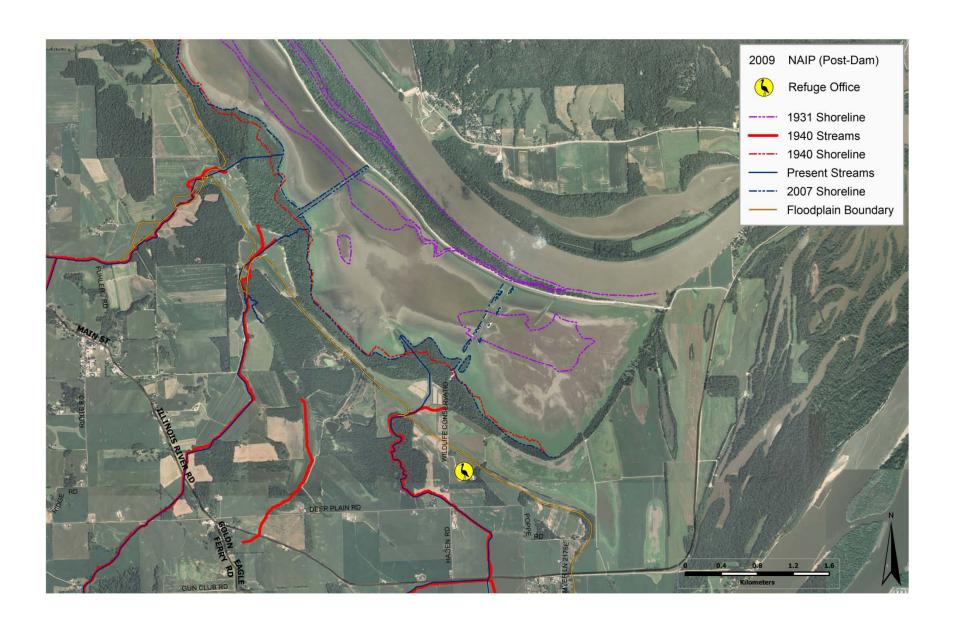












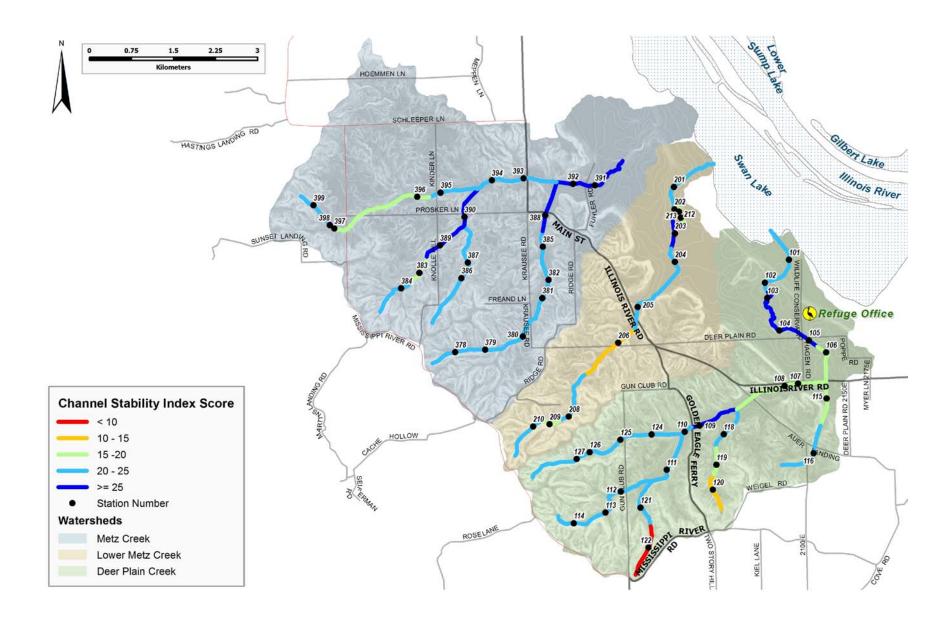
# Appendix C: Channel-Stability Ranking Scheme Tables and Maps

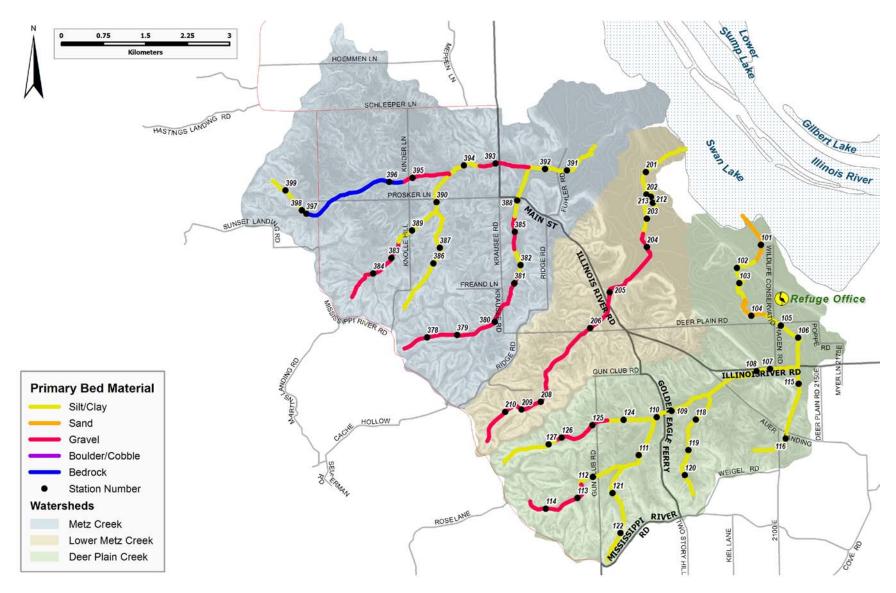
#### **Channel-Stability Ranking Scheme (by station number)**

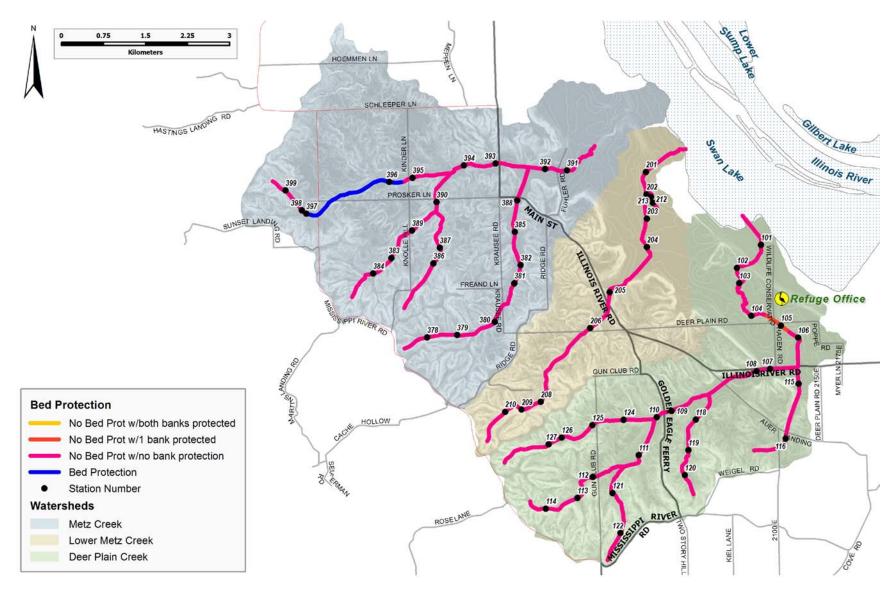
Station	Primary Bed Material	Bed Protection	Floodplain Separation	Degree of Constriction	Type of Bank Erosion LEFT	Type of Bank Erosion RIGHT	Percent Bank Instability (Active) LEFT	Percent Bank Instability (Active) RIGHT	Percent Established Woody Cover LEFT	Percent Established Woody Cover RIGHT	Percent Bank/Bar Accretion LEFT	Percent Bank/Bar Accretion RIGHT	CEM Stage	Channel-Stability Index (CSI)
101	3	1	2	0	2	2	2	2	2	2	2	1	IV	25
102	3.25	1	1	0	1	2	2	2	1.5	1.5	2	1.5	IV-V	22.25
103	4	1	3	0	2	2	2	2	2	2	2	2	IV	28
104	2.5	1	4	0	2	2	2	2	2	2	1.5	1.5	IV	26.5
105	4	2	3	0	1	1	2	2	1.5	1.5	2	2	IV	26
106	4	1	3	0	0	1	0	0	2	2	2	2	111	19
107	4	1	3	0	1	1	0	0	2	2	2	2	111	20
108	4	1 1	3 4	0	0 1	1	0	0	2	2	2	2	111	19
109	4	1	3	0	1	1	0	0	2	2	2	2	IV IV	27 22
111	4	1	4	0	2	2	1	1	1	1	0.5	0.5	V	21
112	4	1	4	0	2	2	1	1	2	2	1	1	V	24
113	2	1	4	0	0	2	0	1	1.5	2	2	2	V	20.5
114	2	i	2	0	2	2	1	1	2	2	2	2	ĪV	23
115	4	i	2	0	1	1	0	Ö	2	2	2	2	11-111	18.5
116	4	1	4	0	1	1	0	0.5	2	2	2	2	11-111	21
118	4	1	3	0	1	1	1	1.5	2	2	2	2		21.5
119	4	1	3	0	1	1	0.5	0.5	1	1	2	2	1	17
120	4	1	3	0	1	1	1	1	0	0	1.5	1.5	1	15
121	4	1	3	0	2	1	2	1	2	0.5	2	2	111	22.5
122	4	1	0	0	0	0	0	0	0	0	0	0	1	5
124	4	1	4	0	2	2	0.5	1.5	1	0.5	2	1	V	22.5
125	2	1	4	0	2	2	1	11	1	1	2	2	IV	23
126	2	1	3	0	2	2	2	1.5	2	1.5	2	2	IV.	25
127	4	1	3	0	1	1	1.5	1.5	2	2	2	2	Ш	23
201	4	1	3	1	1	1	2	2	2	2	2	2	1	24
202	4	i	4	0	1	i	2	2	1.5	2	2	2	IV	26.5
203	4	1	3	0	1	1	2	2	2	2	2	2	IV	26
204	2	1	4	0	1	1	2	2	2	2	2	2	IV	25
205	2	1	4	0	1	1	2	2	2	2	2	2	IV	25
206	2	1	4	0	1	1	0.5	0.5	1	0.5	1	1	11-111	15
208	2	1	4	0	1	1	2	2	2	2	2	2	IV	25
209	2	1	3	0	1	1	0	0	2	0	2	2	III	16
210	2	1	4	0	1	1	2	2	2	2	2	2	IV	25
212	4	1	3	0	1	1	0	0	1.5 2	2	2	2	11-111	19 19.5
213	4	1	3	U	l I	9	U	U	2			2	11-111	19.5
378	2	1	4	0	1	1	2	2	2	1.5	1.5	2	V	23
379	2	i	4	0	i	i	2	2	0.5	2	1	1.5	v	21
380	2	1	4	0	1	1	2	2	1.5	2	1.5	2	V	23
381	2	1	4	0	2	2	1	0.5	2	1	1.5	1.5	V	21.5
382	4	1	4	0	2	2	1	1	2	2	1	1	V	24
383	2	1	4	0	1	1	2	2	1.5	1.5	11	1.5	11-111	20
384	2	1	4	0	2	1	2	2	-1	0.5	1.5	1.5	V	21.5
			7	0.70					7.50	100				
385	2	1	4	0	2	2	2	1.5	2	1.5	1.5	1.5	V	24
386	2	1	4	0	1	1	1.5	1	0.5	1	2	2	V	22
386 387	2 4 4	1 1	4	0 0 0	1	1	1.5 2	1	0.5 0	1	2	2	V IV	22 23
386 387 388	2 4 4 4	1 1 1	4 4 4	0 0 0 0	1 1 1	1 1 1	1.5 2 2	1 1 2	0.5 0 2	1 1 0.5	2 2 2	2 2 2	V IV IV	22 23 25.5
386 387 388 389	2 4 4 4 4	1 1 1 1	4 4 4 4	0 0 0 0	1 1 1	1 1 1	1.5 2 2 2	1 1 2 2	0.5 0 2 1	1 1 0.5 1.5	2 2 2 2	2 2 2 2	V IV IV	22 23 25.5 25.5
386 387 388 389 390	2 4 4 4 4 4	1 1 1 1 1	4 4 4 4 4	0 0 0 0 0	1 1 1 1	1 1 1 1 1	1.5 2 2 2 2	1 1 2 2 2	0.5 0 2 1 1.5	1 0.5 1.5 1.5	2 2 2 2 2	2 2 2 2 2	V IV IV	22 23 25.5 25.5 26
386 387 388 389 390 391	2 4 4 4 4	1 1 1 1	4 4 4 4	0 0 0 0	1 1 1 1 1	1 1 1 1 1	1.5 2 2 2 2 2 2	1 1 2 2 2 2	0.5 0 2 1 1.5 1.5	1 0.5 1.5 1.5	2 2 2 2 2 2	2 2 2 2 2 2	V IV IV	22 23 25.5 25.5 26 26.5
386 387 388 389 390	2 4 4 4 4 4 4	1 1 1 1 1 1	4 4 4 4 4 4	0 0 0 0 0 0	1 1 1 1	1 1 1 1 1	1.5 2 2 2 2	1 1 2 2 2	0.5 0 2 1 1.5	1 0.5 1.5 1.5	2 2 2 2 2	2 2 2 2 2	V	22 23 25.5 25.5 26
386 387 388 389 390 391 392	2 4 4 4 4 4 4 4	1 1 1 1 1 1 1 1 1	4 4 4 4 4 4 4	0 0 0 0 0 0	1 1 1 1 1 1 2	1 1 1 1 1 1 2	1.5 2 2 2 2 2 2 2	1 1 2 2 2 2 2 2	0.5 0 2 1 1.5 1.5	1 0.5 1.5 1.5 2	2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2	V	22 23 25.5 25.5 26 26.5 28
386 387 388 389 390 391 392 393	2 4 4 4 4 4 4 4 2	1 1 1 1 1 1 1 1 1 1 1	4 4 4 4 4 4 4	0 0 0 0 0 0 0	1 1 1 1 1 1 2	1 1 1 1 1 1 2	1.5 2 2 2 2 2 2 2 2 2	1 1 2 2 2 2 2 2 2 2	0.5 0 2 1 1.5 1.5 2	1 0.5 1.5 1.5 2 2	2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2	V IV IV IV IV	22 23 25.5 25.5 26 26.5 28 22
386 387 388 389 390 391 392 393 394	2 4 4 4 4 4 4 4 2 3.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4 4 4 4 4 3	0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 2 0	1 1 1 1 1 1 2 1 1 1 1 2	1.5 2 2 2 2 2 2 2 2 0 2	1 1 2 2 2 2 2 2 2 2 2 2	0.5 0 2 1 1.5 1.5 2 2	1 0.5 1.5 1.5 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	V	22 23 25.5 25.5 26 26.5 28 22 25
386 387 388 389 390 391 392 393 394 395 396 397	2 4 4 4 4 4 4 2 3.5 2 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0	4 4 4 4 4 4 4 3 4 4	0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 2 0 1 1 1 1	1 1 1 1 1 1 2 1 1 1 1 2	1.5 2 2 2 2 2 2 2 0 2 2 2 1.5 2	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.5 0 2 1 1.5 1.5 2 2 2 1.5 1.5	1 0.5 1.5 1.5 2 2 2 2 2 2 1 0.5	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	V	22 23 25.5 25.5 26 26.5 28 22 25 23.5 17
386 387 388 389 390 391 392 393 394 395 396	2 4 4 4 4 4 4 4 2 3.5 2	1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4 4 4 4 4 3 4	0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 2 0 1 1 1	1 1 1 1 1 1 2 1 1 1 1 2	1.5 2 2 2 2 2 2 2 0 2 2 2 1.5	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.5 0 2 1 1.5 1.5 2 2 2 1.5 1.5	1 0.5 1.5 1.5 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	V	22 23 25.5 26.5 26 26.5 28 22 25 23.5

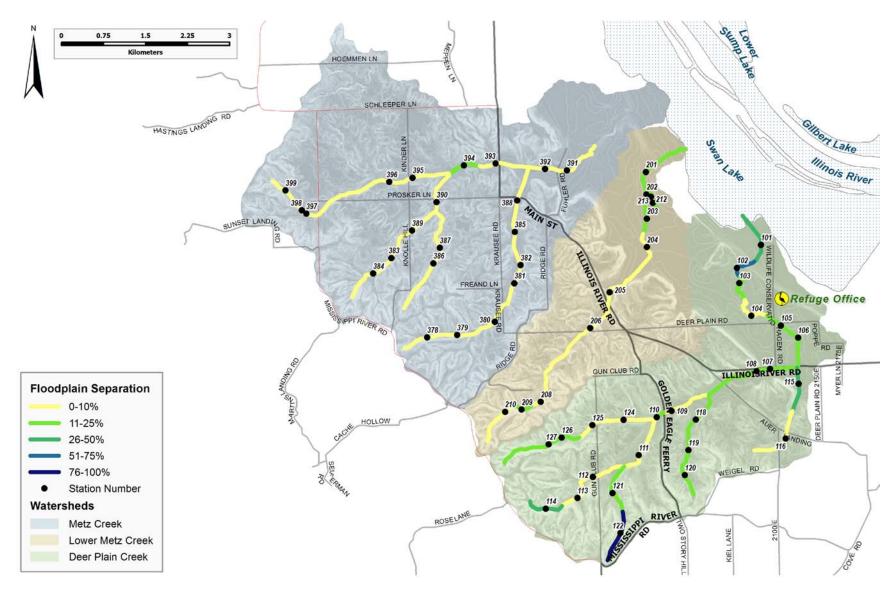
#### Channel-Stability Ranking Scheme (by CSI score)

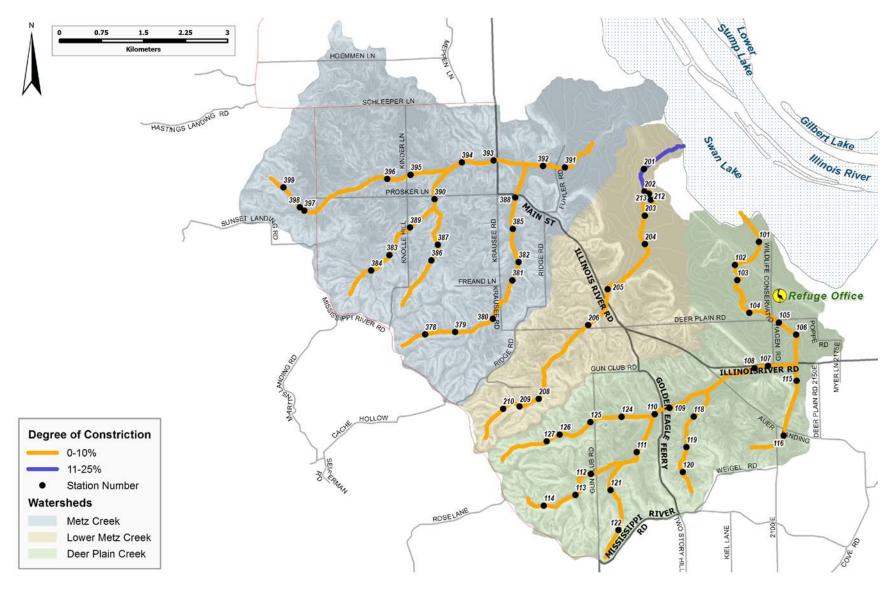
Station	Primary Bed Material	Bed Protection	Floodplain Separation	Degree of Constriction	Type of Bank Erosion LEFT	Type of Bank Erosion RIGHT	Percent Bank Instability (Active) LEFT	Percent Bank Instability (Active) RIGHT	Percent Established Woody Cover LEFT	Percent Established Woody Cover RIGHT	Percent Bank/Bar Accretion LEFT	Percent Bank/Bar Accretion RIGHT	CEM Stage	Channel-Stability
103 109	4	1	3	0	2	2	2 2	2 2	2	2	2	2	IV IV	28 27
109	2.5	1	4	0	2	2			2	2	1.5	1.5	IV	26.5
105	4	2	3	0	1	1	2 2 2	2 2 2	1.5	1.5	2	2	IV	26
101	3	1	2	0	2	2	2	2	2	2	2	2	IV	25
126 112	2 4	1	3	0	2	2 2	2	1.5 1	2	1.5	2	2	IV V	25
114	2	1	2	0	2	2	1	1	2	2 2	2	2	IV	26 25 25 24 23 23
125	2	1	4	0	2	2	1	1	1	1	2	2	IV	23
127	4	1	3	0	1	1		1.5	2	2	2	2	111	23 22.5
121 124	4	1	3	0	2	1 2	0.5	1.5	2	0.5 0.5	2	2	III V	22.5
102	3.25	1	1	0	1	2	2		1.5	1.5	2	1.5	IV-V	22.25
110	4	1	3	0	1	1	0	2 0	2	2	2	2	IV	22
118	4	1	3	0	1	1	1	1.5	2	2	2	2		21.5
111 116	4	1	4	0	2	2 1	1 0	0.5	1 2	1 2	0.5	0.5	V   -	21 21
113	2	1	4	0	0	2	0	1	1.5	2	2	2	V	20.5
107	4	1	3	0	1			0	2	2	2	2	111	20
106 108	4	1	3	0	0	1	0	0	2 2	2	2 2	2	111	19 19
115	4	1	2	0	1	i	0	0	2	2	2	2	11-111	18.5
119	4	1	3	0	1	1	0.5	0.5	1	1	2	2	1	17
120	4	1	3	0	1	1	1	1	0	0	1.5	1.5	1	15 5
122	4	1	0	0	0	0	0	0	0	0	0	0	I,	5
202	4	1	4	0	1	1	2	2 2	1.5	2	2	2	IV	26.5
203 204	4 2	1	3 4	0	1	1		2	2 2	2 2	2 2	2 2	IV IV	26 25 25 25 25 25 25 24
204	2	1	4	0	1	1	2	2 2	2	2	2	2	IV	25
208	2	1	4	0	1	1	2		2	2	2	2	IV	25
210	2	1	4	0	1		2	2 2 2	2	2	2	2	IV	25
201 213	4	1	3	1 0	1	1	2 0	0	2	2 2	2 2	2	11-111	19.5
212	4	1	3	0	1	1	0	0	1.5	2	2	2	11-111	19
209	2	1	3	0	1	1	0	0	2	0	2	2	111	16
206	2	1	4	0	1	1	0.5	0.5	1	0.5	1	1	11-111	15
392	4	1	4	0	2	2		2	2	2	2	2	V	28
391	4	1	4	0	1	1	2	2	1.5	2	2	2	IV	26.5
390 388	4	1	4	0	1	1	2	2 2	1.5 2	1.5 0.5	2	2	IV IV	26 25.5
389	4	1	4	0	1	1	2	2	1	1.5	2	2	iv	25.5
394	3.5	1	3	0	1	1	2	2	2	2	2	2	IV-V	25
398 399	3.75	1	4	0	1	1	2	2 2	2	2	2	2	III	25 24.75
382	3.73	1	4	0	2	2		1	2	2	1	1	V	24.73
385	2	1	4	0	2	2	2	1.5	2	1.5	1.5	1.5	V	24
395	2	1	4	0	1	1		2	1.5	2	2	2	V	23.5
378 380	2	1	4	0	1	1	2	2 2	1.5	1.5	1.5 1.5	2	V	23 23
387	4	1	4	0	1	1	2	1	0	1	2	2	ΙV	23
386	4	1	4	0	1	1	1.5	1	0.5	1	2	2	V	22
393 381	2	1	4	0	0 2	1	0	0.5	2	2	1.5	1.5	IV V	22 21.5
384	2	1	4	0	2	<u>2</u> 1		2	1	0.5	1.5	1.5	V	21.5
379	2	1	4	0	1	1	2	2	0.5	2	1	1.5	V	21
383	2	1	4	0	1			2	1.5	1.5	1	1.5	11-111	20
397 396	0	0	4	0	1	1 2		2 2	1.5	0.5	1.5	1.5	V	17.5 17
390	U	U	4	U		2	1.5	2	1.5	- 1	4	2	- II	17

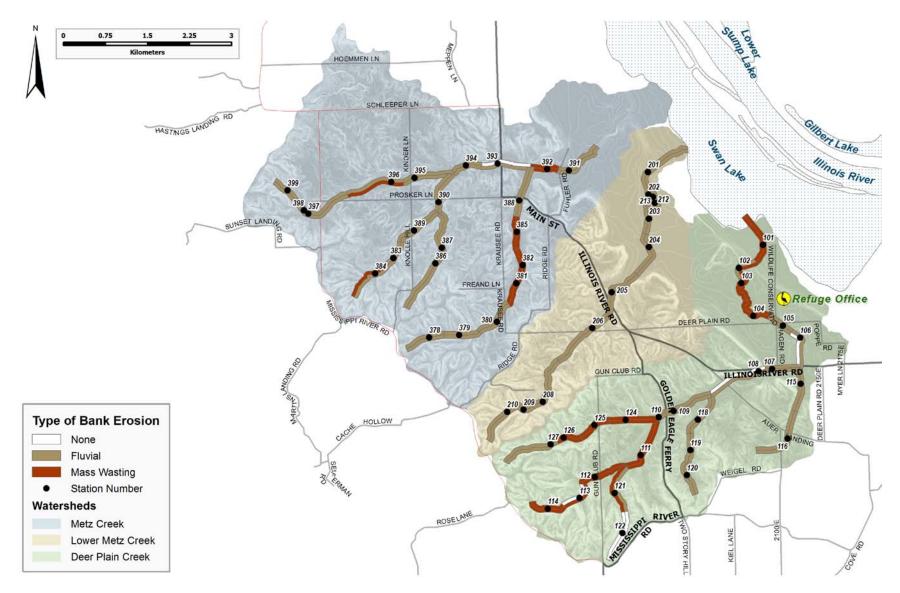


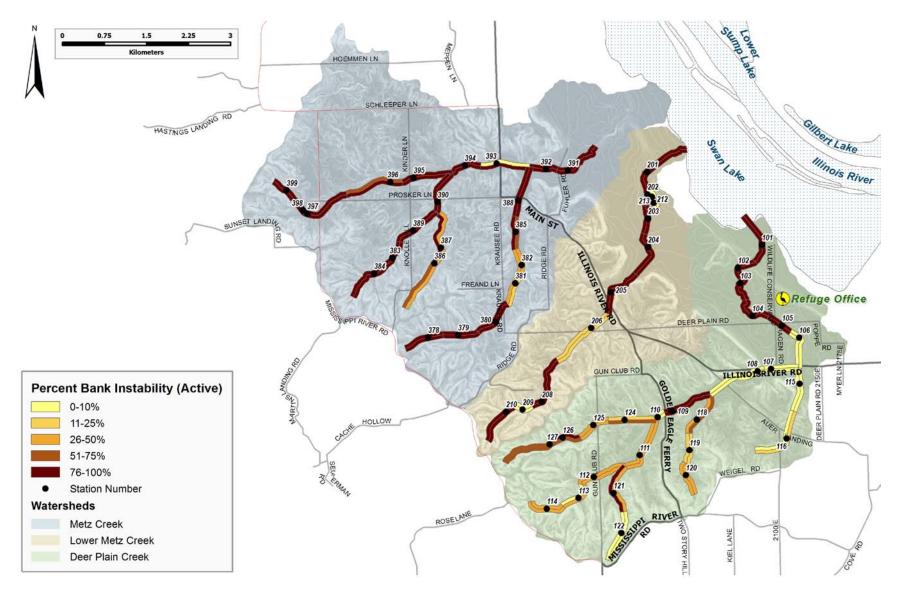


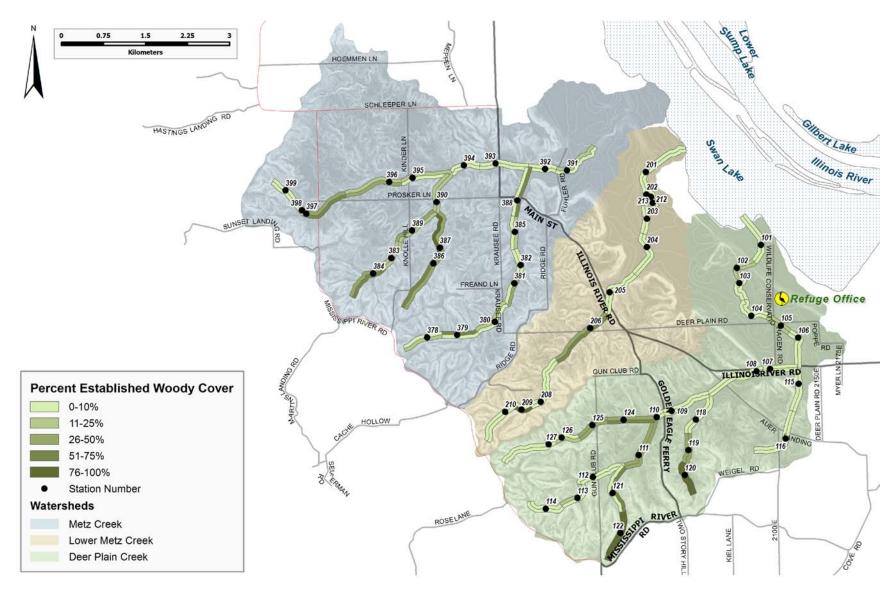


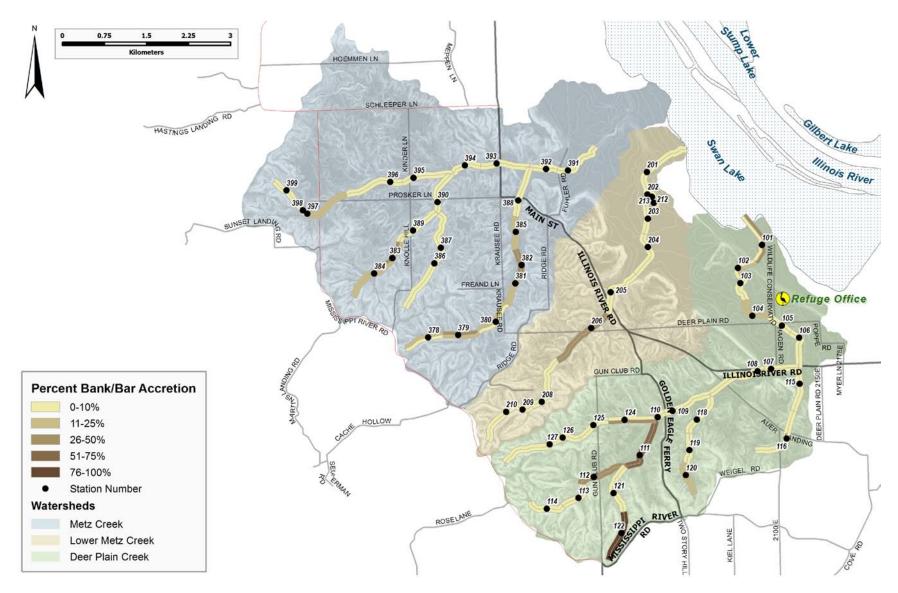


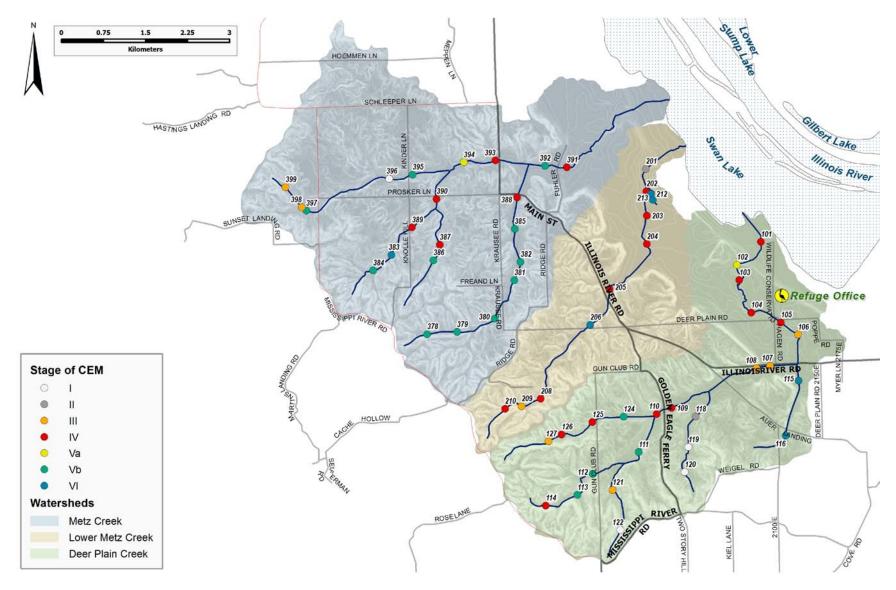


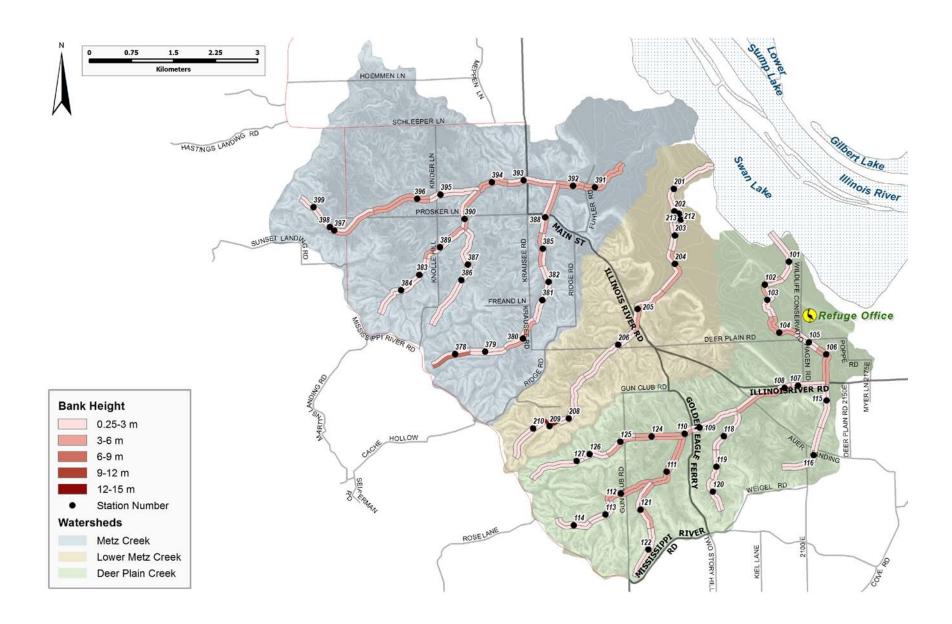


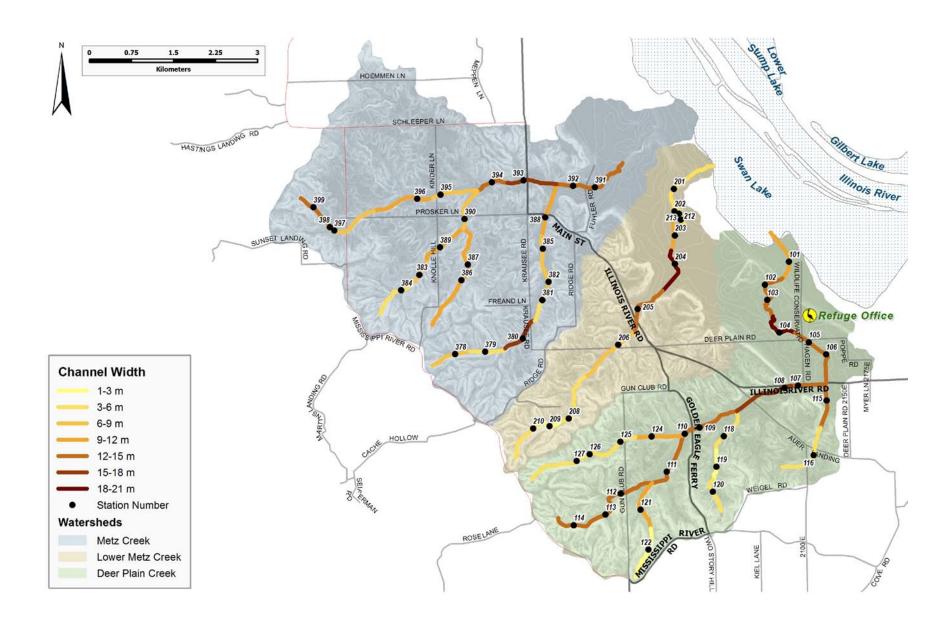


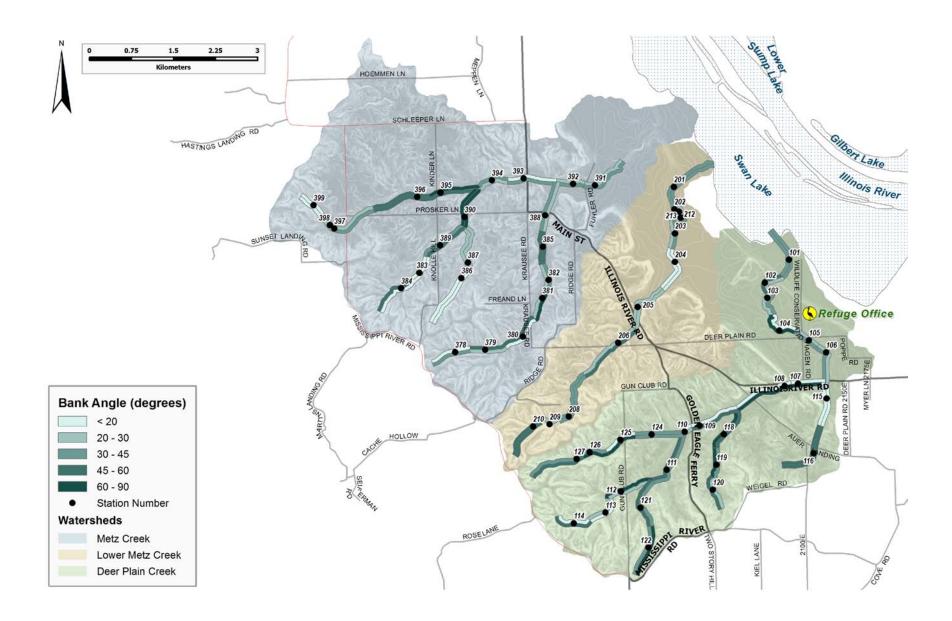












## Appendix D: Biological/Habitat Ranking Scheme Tables and Maps

## **Biological/Habitat Ranking Scheme (by station number)**

Station	Availability of Favorable Habitat	Active streambed/bar deposition	Percent Streambed Exposure	Degree of "Hard" Channel Alteration	Percent Bank Instability LEFT	Percent Bank Instability RIGHT	Vegetative Bank Protection(Bank Face) LEFT	Vegetative Bank Protection(Bank Face) RIGHT	Riparian-zone Width (out from edge of water) LEFT	Riparian-zone Width (out from edge of water) RIGHT	Biological/Habitat
101	1	4	4	1	0.5	0.5	0.5	0.5	0.5	0.5	17
102	1	4	4	4	0.5	0.5	0.5	0.5	1.5	2	26 23 27 19 24 22 22.5
103	1	4	4	4	0.5	0.5	0.5	0.5	2	2	23
104 105	1	4	4	4	0.5 0.5	0.5 0.5	0.5 0.5	0.5 0.5	1 0.5	0.5 0.5	10
103	1	4	4		2	2	0.5	2	0.5	0.5	24
107	1	4	4	2	2	2	2 1.5	2 0.5	0.5	0.5	22
108	1	4	4	3 2 3	2 2 2	2 2 2	2	0.5	0.5	0.5	22.5
109	1	4	4	4	0.5	0.5	1	1	0.5	0.5	20 23.5
110	1	4	4	4	2	2	1	1.5	0.5	0.5	23.5
111	3	3 3	3	4	1	1	1	1	0.5	0.5	27 22.5
112 113	1		4	3	1	1	1	1	0.5	0.5	22.5
113	1	4	4	4	2	1.5 1	2 1	1	0.5 0.5	0.5 0.5	26.5 28
115	4	4	4	4	2	2	2	2	0.5	0.5	28
116	2	4	4	3	1.5	1.5	1	1	0.5	0.5	22
118 119	1	4	4	1	1	0.5	0.5	0.5	0.5	0.5	22 17.5 28.5
119	2	4	4	3	2	0.5 1.5	1.5	1.5	0.5	0.5	28.5
120	4 2	3	3 4	4	1	1	2 0.5	2	0.5	0.5	29 27
121	2	4	4	4	0.5	1	0.5	2	0.5	0.5	27
122 124	1	1	3	4	2 1.5	2	2	2	2 0.5	2	29 27.5
125	3	3 4	3	3 4	1.5	1	1	1	0.5	0.5 0.5	27
126	2 2 2	3	2 2	4	0.5	0.5	0.5	0.5	2	1	25
127	2	4	4	4	1	1	0.5	0.5	2 0.5	2	25 25.5
201	1	4	4	1	0.5	0.5	0.5	0.5	0.5	0.5	16
202	1	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	19
203	1	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	19
204 205	1	4	4	4	0.5 0.5	0.5 0.5	0.5 1.5	1	0.5 0.5	0.5 0.5	19 19 20.5 21.5
205	2 3 1	3	4	3	1.5	1.5	1.5	2	0.5	0.5	28.5
206 208	1	4	4	4	1.5 0.5	1.5 0.5	1.5 0.5	0.5	1	2	21
209	1	4	4	4	2	1.5	0.5	0.5	0.5	0.5	22.5
210	2	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	22
212	1	4	4	4	1.5	1.5	0.5	0.5	0.5	0.5	21.5
213	1	4	4	4	1.5	2	0.5	0.5	0.5	0.5	21.5
378	1	3	4	4	0.5	0.5	0.5	0.5	2	1	22
379	1	3 2	4	4	0.5 0.5	0.5 0.5	1	0.5	1	0.5	22 21 23 25
380	1	3	4	4	0.5	0.5	0.5	0.5	2	2	23
381	1	4	4	4	2	1	1	1.5	0.5	1	25
382	1	4	4	3	1	1	1.5	1.5	0.5	0.5	22
383 384	2	2	4	4	0.5	0.5 0.5	0.5	0.5 0.5	0.5	0.5 0.5	20.5
385	1 2	4	4	4	0.5	1	0.5	0.5	0.5 0.5	0.5	20 26
386	2	4	4	3	1.5	1.5	1	1	0.5	0.5	27
387	2	4	4	3	0.5	2	1	1	0.5	0.5	26.5
388	1	4	4	3	0.5	0.5	0.5	1	0.5	0.5	23.5
389	2	4	4	3	0.5	0.5	1	0.5	0.5	0.5	22.5
390	1	4	4	3	0.5	0.5	0.5	0.5	0.5	0.5	20
391 392	1	1 4	4	3	0.5 0.5	0.5	1	0.5	0.5	0.5	21.5
392	1	4	4	4	2	0.5 0.5	0.5 2	0.5 0.5	0.5 0.5	0.5 0.5	24.5
394	1	4	4	4	0.5	0.5	1	0.5	1	0.5	24.5
395	1	4	4	4	0.5	0.5	1	0.5	0.5	0.5	27
396	3	4	2	4	1	0.5	1	0.5	1	0.5	24
397	1	3	2	3	0.5	0.5	0.5	1	0.5	0.5	20.5
398	3.5	4	4	4	0.5	0.5	0.5	0.5	1 75	0.5	23.5
399	3.5	4	2	4	0.5	0.5	0.5	0.5	1.75	1	23.75

## **Biological/Habitat Ranking Scheme (by BHI score)**

otation Station 120	Availability of Favorable Habitat	Active streambed/bar deposition	Percent Streambed Exposure	Degree of "Hard" Channel Alteration	Percent Bank Instability LEFT	Percent Bank Instability RIGHT	Vegetative Bank Protection(Bank Face) LEFT	Vegetative Bank Protection(Bank Face) RIGHT	Riparian-zone Width (out from edge of water) LEFT	Riparian-zone Width (out from edge of water) RIGHT	Biological/Habitat 62   62   Index (BHI)
120	4	3	3	4	1	1	2 2 1.5	2 2 1.5	0.5	0.5	29
122 119	1 2	1 4	3 4	4	2	2 1.5	15	15	0.5	2 0.5	28.5
114	1	3	4	4	1	1.0	1.0	1.0	0.5	0.5	28
114 115	4	4	4	4	1.5	2	2	1 2	0.5 0.5	0.5	28
124 104	3	3	3	3	1.5 0.5	0.5	0.5	0.5	0.5	0.5 0.5	27.5
111	1 3	4	4 3	4	1	1	0.5	1	0.5	0.5	28 27.5 27 27 27 27 27 26.5 26.5 25.5 24
121	2	4	4	4	0.5	1	0.5	2	0.5	0.5	27
125	2	4	2	4	1	1	1	1	0.5	0.5	27
113 102	1	4	4	4	2 0.5	1.5	2 0.5	1	0.5	0.5	26.5
102	1	4	4	4	1	0.5	0.5	0.5	1.5 0.5	2 2 1	25.5
126	2 2	3	2	4	0.5	0.5	0.5 0.5	0.5 0.5	2	1	25
106	1	4	4	3	2	2	2	2 1.5	0.5	0.5	24
110	1	4	4	4	2 0.5	2 0.5	1	1.5	0.5	0.5	23.5 23 22.5
103 108	1	4	4	4 3	0.5	0.5	0.5 2	0.5 0.5	2 0.5	2 0.5	23
112	1	3	4		1	1	1	0.3	0.5	0.5	22.5
112 107	1	4	4	3 2 3	1.5	2 1.5	1.5	1 0.5	0.5	0.5 0.5	22.5 22
116	2	4	4		1.5	1.5	1	1	0.5	0.5	22 20 19 17.5
109 105	1	4	4	4	0.5 0.5	0.5 0.5	1 0.5	1	0.5	0.5 0.5	20
118	1	4	4	1	1	0.5	0.5	0.5 0.5	0.5 0.5 0.5	0.5	17.5
101	1	4	4	1	0.5	0.5 0.5	0.5	0.5	0.5	0.5	17
		-1									
206 209	3	3	4	3 4	1.5	1.5 1.5	1.5 0.5	0.5	0.5 0.5	0.5 0.5	28.5
210	2	4	4	4	2 0.5	0.5	0.5	0.5	0.5	0.5	22.3
205	2	4	4	4	0.5	0.5	1.5	1	0.5	0.5	21.5
213	1	4	4	4	1.5	2 0.5	0.5	0.5	0.5	0.5	22.5 22 21.5 21.5
208 212	1	4	4	4	0.5 1.5	0.5 1.5	0.5 0.5	0.5 0.5	0.5	2 0.5	21 21
204	1	4	4	4	0.5	0.5	0.5	1	0.5	0.5	20.5
202	1	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	20.5
203	1	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	19 16
201	1	4	4	1	0.5	0.5	0.5	0.5	0.5	0.5	16
386	2	4	4	3	1.5	1.5	1	1	0.5	0.5	27
395	2	4	4	4	0.5	0.5	1	0.5	0.5	0.5	27 27
387	2	4	4	3	0.5	2	1	1	0.5	0.5	26.5 26
385 381	1	4	4	4	0.5 2	1	0.5 1	0.5 1.5	0.5 0.5	0.5 1	25
393	1	4	4	4	2	0.5	2	0.5	0.5	0.5	24.5
394	1	4	4	4	0.5	0.5	1	0.5	1	0.5	24.5
396	3	4	2	4	1	0.5	1	0.5	1 75	0.5	24
399 388	3.5	4	2 4	4	0.5 0.5	0.5 0.5	0.5 0.5	0.5	1.75 0.5	0.5	23.75
398	3.5	4	4	4	0.5	0.5	0.5		1	0.5	23.5
380	1	3	4	4	0.5	0.5	0.5	0.5	2	2	23
389	2	4	4	3	0.5	0.5	1	0.5	0.5	0.5	22.5
378 382	1	3 4	4	3	0.5 1	0.5	0.5 1.5	0.5 1.5	0.5	0.5	22 22
391	1	1	4	3	0.5	0.5	1.3	0.5	0.5	0.5	21.5
379	1	2	4	4	0.5	0.5	1	0.5	1	0.5	21
392	1	4	4	4	0.5	0.5	0.5	0.5	0.5	0.5	21
383 397	2	2	4	3	0.5 0.5	0.5 0.5	0.5	0.5 1	0.5 0.5	0.5 0.5	20.5
384	1	3	4	4	0.5	0.5	0.5	0.5	0.5	0.5	20.3
390	1	4	4	3	0.5	0.5			107,144,000		20

